

# A Computational Approach to Aircraft Engine Noise Propagation and Scattering

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## Field Method Approaches

- Time-domain Linear/Nonlinear Model
  - Advantages: all frequencies up to the limit of the resolution can be modeled together in a single run; requires smaller amount of computer memory.
  - Disadvantages: possibly larger wall-clock time for one run; stability for viscous mean flow unclear.
- Frequency-domain Linear Model
  - Advantages: can produce faster results for a single frequency.
  - Disadvantages: needs large amounts of computer memory to store and solve the complex linear algebra problem.

## Time-domain Nonlinear Model

- The nonlinear inviscid flow (Euler) equations

$$\frac{\partial Q}{\partial t} + \sum_{d=1}^3 \frac{\partial F_d}{\partial x_d} = 0$$

$$Q = \begin{pmatrix} \rho \\ \rho v_1 \\ \rho v_2 \\ \rho v_3 \\ \rho E \end{pmatrix}, \quad F_d = \begin{pmatrix} \rho v_d \\ \rho v_1 v_d + p \delta_{1d} \\ \rho v_2 v_d + p \delta_{2d} \\ \rho v_3 v_d + p \delta_{3d} \\ (\rho E + p) v_d \end{pmatrix}$$

are considered to govern noise propagation.

- Solution  $Q$  is searched in a trial space of orthogonal three-dimensional polynomials (spectral approximation)

$$Q(t, x, y, z) = \sum_{i=0}^N \sum_{j=0}^N \sum_{k=0}^N Q_{ijk}(t) h_i(x) h_j(y) h_k(z)$$

- After a Galerkin projection, the governing equations are reduced to

$$\frac{dQ_{ijk}}{dt} = - [D^x + D^y + D^z] \mathbf{F}$$

where the right-hand side is a sum of discrete differential operators evaluated numerically.

- These equations represent a system of ODEs for  $Q_{ijk}$  that is integrated in time using a  $2N$ -storage wave-optimized Runge-Kutta method.

## Acoustic computations strategy

- First the (inviscid) mean flow is computed using the same method/grid subject to steady-state boundary conditions, and stored in memory.
- The total flow field variables are then computed using time-dependent boundary conditions that specify the incoming modes; acoustic variables can be obtained by subtracting the mean flow.
- For a viscous mean flow  $\mathbf{F}_0$  (obtained by other solvers, not a solution to the governing equations), the same nonlinear model can be used by subtracting  $[D^x + D^y + D^z] \mathbf{F}_0$  from the RHS of the equations. **Stability is being investigated.**

## Parallelization strategy

- The DG method is highly parallelizable using the message-passing strategy: information between neighboring elements needs to be known only on element faces (lower dimensional manifold.)
- Overlapping of communication and computation is possible by first computing and communicating fluxes in elements near the partition boundaries. The other elements computed while communication proceeds.
- Good speed-ups have been obtained even on small grids (884 elements on 16 processors; grid decomposed using the multilevel strategy in METIS).

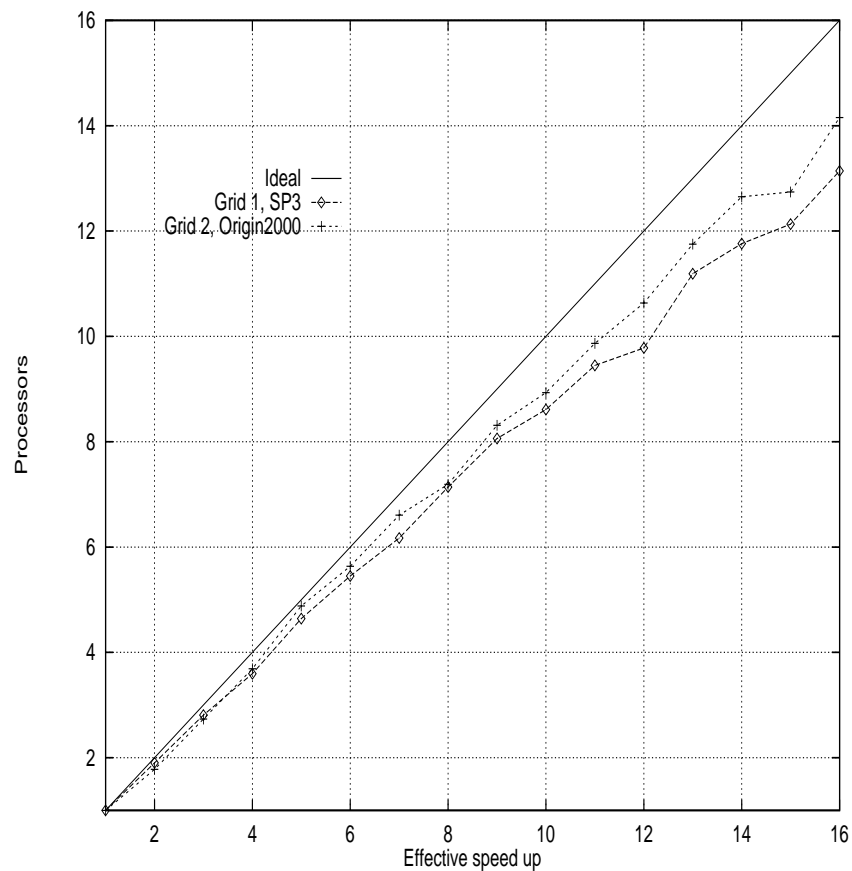


Figure 1: Parallel performance for two test cases. Grid 1: 884 elements. Grid 2: 17,370 elements. "Bad" performance (grid 2 on 15 processors) due to "bad" domain decomposition (many cut faces).

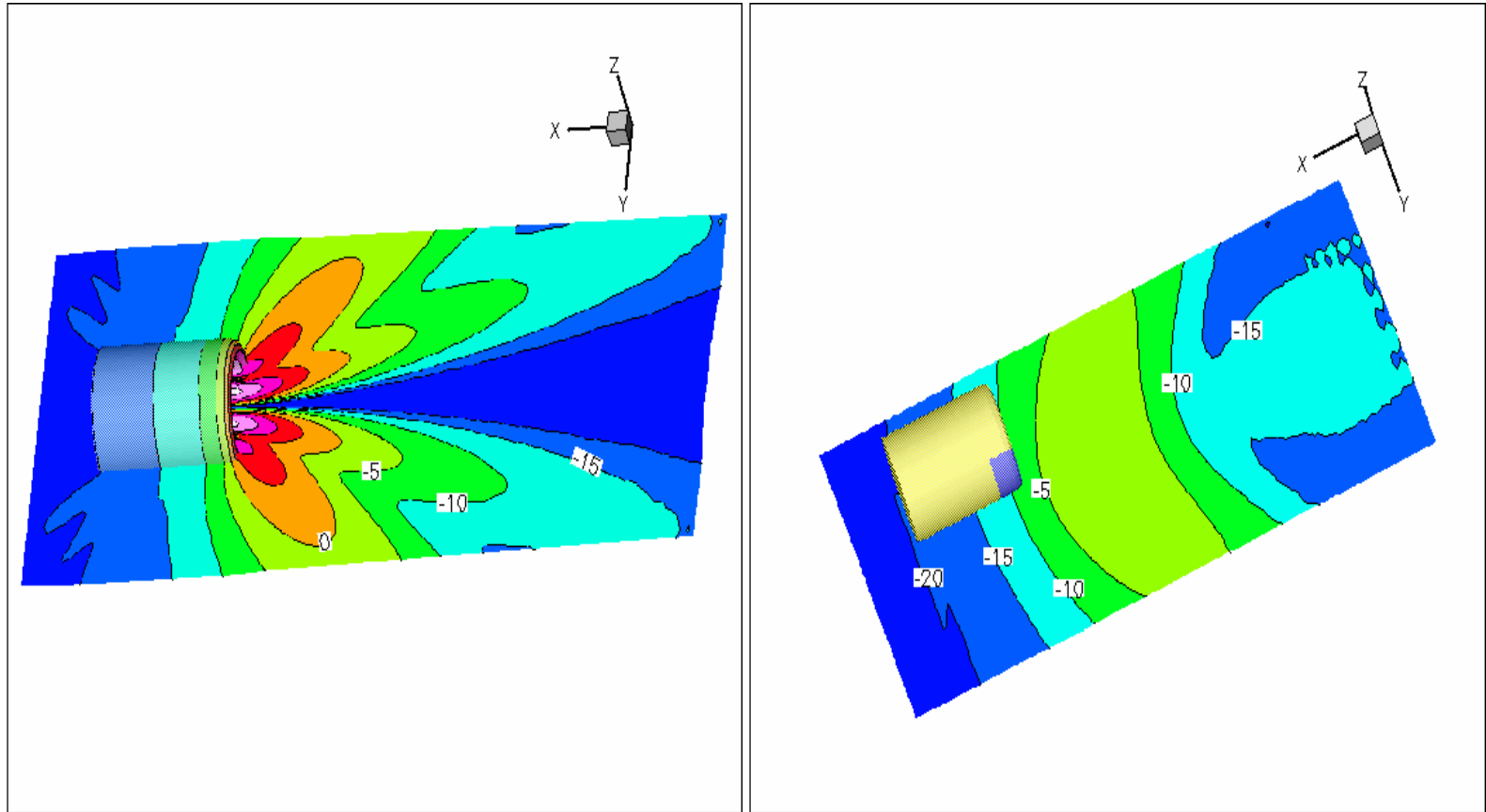


Figure 2: SPL contours for radiation of spinning mode  $(2,1)$  from an axisymmetric bell-mouth nacelle at reduced frequency  $\omega = 8.0$  and  $M_\infty = 0$ . Nacelle surface and plane through its axis (left); plane  $z = -4$  (right). 3,402,217 discretization points.



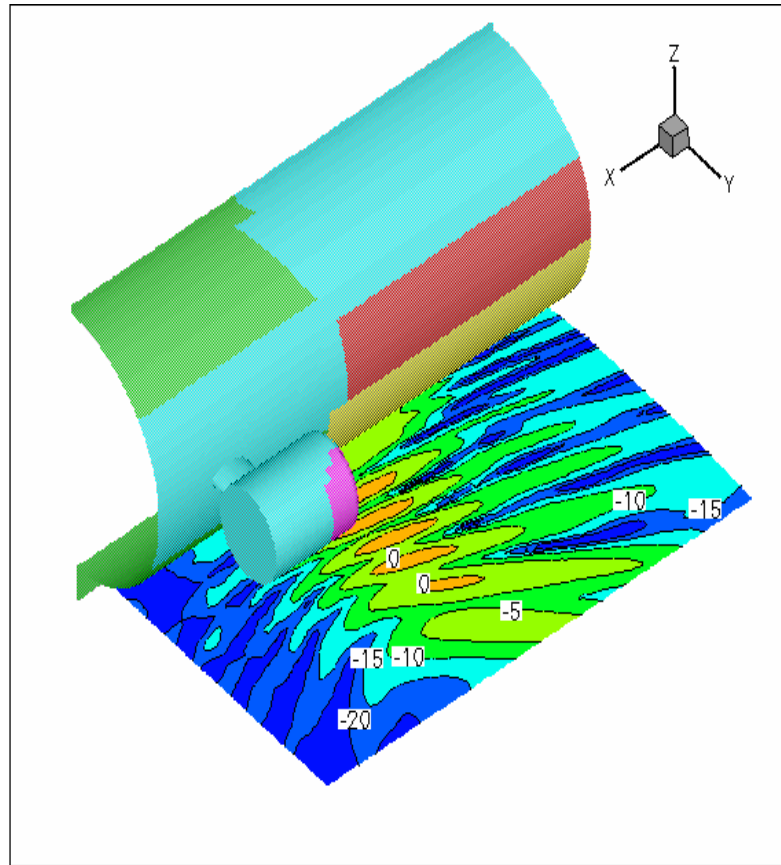


Figure 3: SPL contours for the same case when the nacelle is mounted on a fuselage, plane  $z = -4$ . Trace of mesh decomposition shown on the solid surfaces. 5,957,910 discretization points.

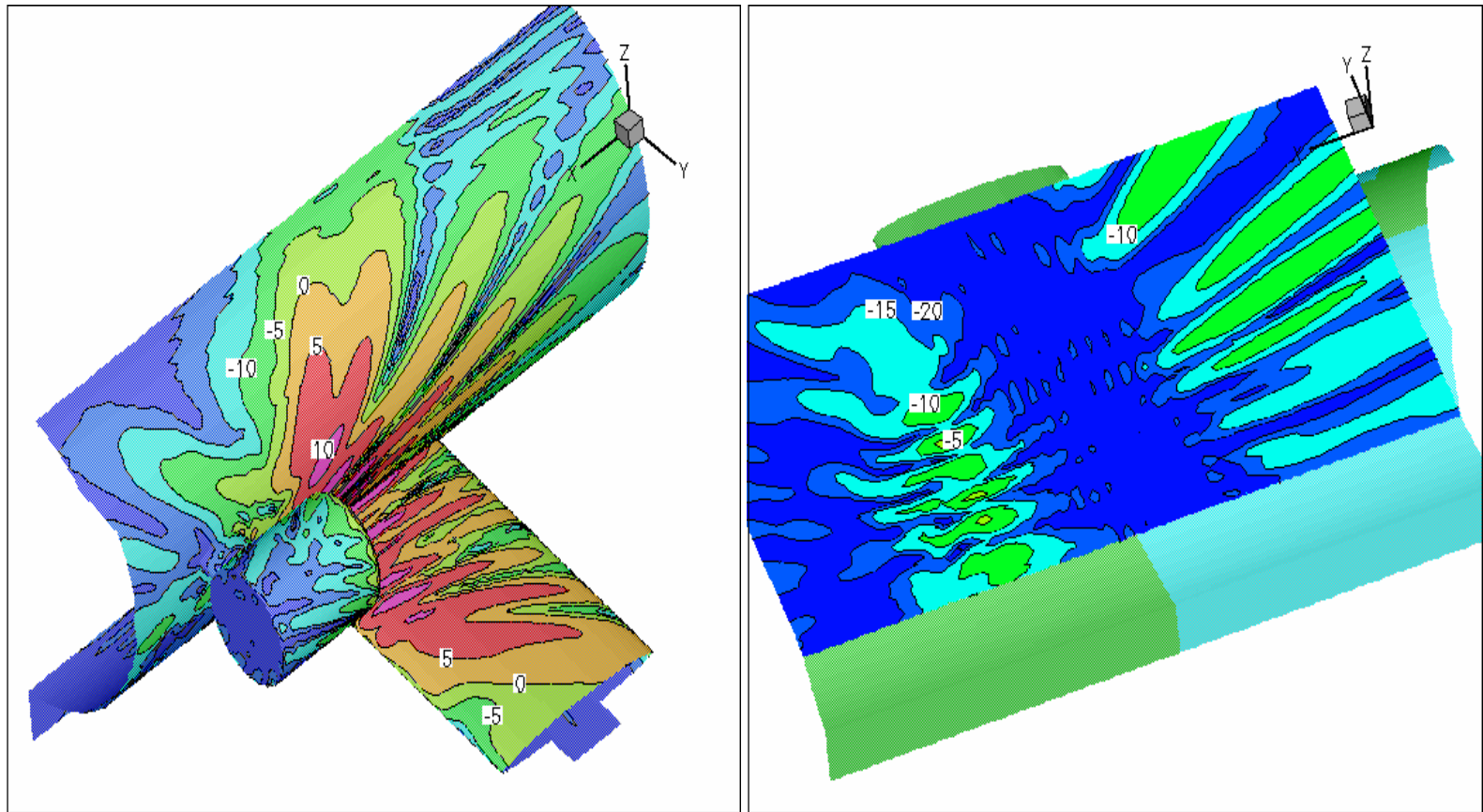


Figure 4: SPL contours for the same case when a wing is added to the configuration. Solid surfaces (left); plane  $z = -4$  seen from below (right). 7,835,149 discretization points.

## Conclusions and Future Development

- Largest run to date: 7,835,149 points, 39,000,000 DOFs, 1.5GB storage (reduced frequency  $\omega=8.0$ ); 250 hrs. run on 16 processors, IBM SP3 at 375MHz.
- For industrial use at around  $\omega=20.0$ , must fine-tune the code for improved performance.
- Current radiation boundary conditions (damping layer type) do not always perform well at domain corners (i.e. Fig. 4 left, upper-right corner).
- Multiple sources (engines), improved radiation boundary conditions and viscous flow capability to be added.